

Hybrid Silicon DQPSK Receiver

Kimchau N. Nguyen¹, Stefano Faralli^{1,2}, Hui-Wen Chen¹, Jon D. Peters¹, John M. Garcia¹, John E. Bowers¹,
Daniel J. Blumenthal¹

¹Electrical and Computer Engineering Department, University of California, Santa Barbara CA 93106

²Scuola Superiore Sant'Anna, 56124 Pisa, Italy
kim@ece.ucsb.edu

Abstract: We present a monolithic 50 Gb/s DQPSK receiver on hybrid silicon, consisting of delay interferometers, phase shifters, balanced InGaAs p-i-n photodetectors, and MIS capacitors. Preliminary measurements of stand-alone PDs show 23-28 GHz 3dB bandwidth.

1. Introduction

QPSK and DQPSK are becoming more prominent modulation formats due to their increased spectral efficiency compared to OOK and tolerance to chromatic dispersion [1]. QPSK receivers have the benefit of higher sensitivity, but require the use of a local oscillator. DQPSK receivers do not require a low linewidth laser or high speed signal processing for carrier phase estimation due to their differential detection scheme [2]. DQPSK receivers on silicon are of interest for their potential compatibility with low cost, high volume and mature CMOS processes [3].

2. Design

The DQPSK receiver consists of two MMI-based delay interferometers with four NiCr heater phase shifters, two balanced InGaAs p-i-n photodetector pairs, and four on-chip MIS (metal-insulator-semiconductor) capacitors. The mask layout is shown in Fig. 1 (a) and (b) is a photo of the device. The two 40 ps interferometers are to be biased at $\pi/4$ and $-\pi/4$ in order to receive the different signal quadratures.

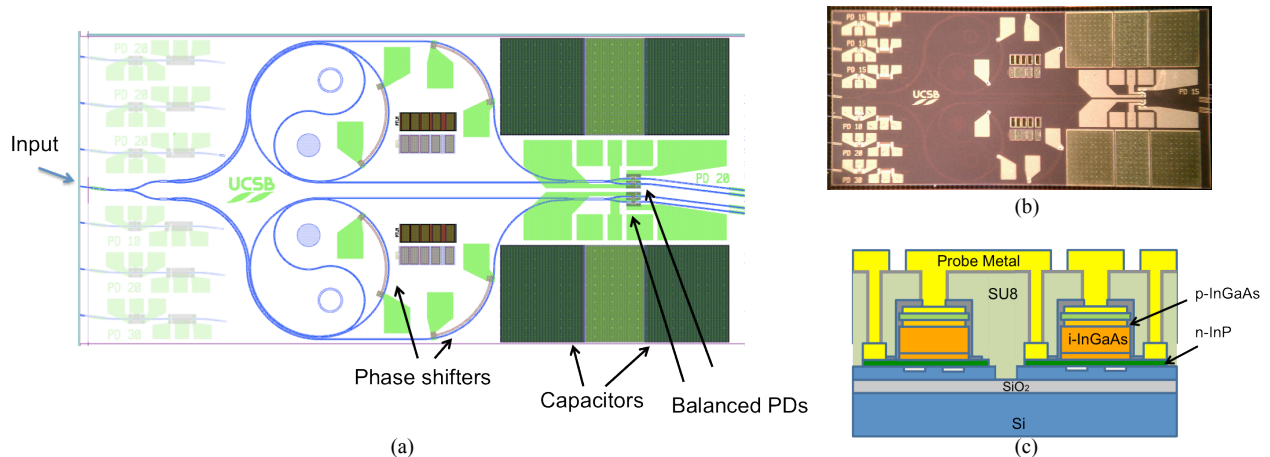


Figure 1. Mask layout of the DQPSK receiver (a). Waveguides are shown in blue, metal contacts are light green. The layout includes stand-alone single PD test structures on the left. Photograph of the receiver PIC (b) and details of the balanced p-i-n InGaAs PD structure (c).

The waveguide structure is SOI with a $0.7 \mu\text{m}$ waveguide height and $0.3 \mu\text{m}$ etch depth. The phase shifters are NiCr heaters $10 \mu\text{m}$ wide and $500 \mu\text{m}$ long. The balanced photodetectors shown in Fig. 1(c) have a similar structure as the single photodetector in [4], with a $0.5 \mu\text{m}$ thick intrinsic InGaAs absorber region. The photodiode lengths of 10, 15, 20, 25, $30 \mu\text{m}$ were chosen for 25 Gbaud operation considering RC and transit time limitations. The on-chip MIS capacitors have 3000 \AA thick SiN as the dielectric, use the n-InP layer as the semiconductor, and are designed to be approximately 50 pF , as large as possible given the space constraints of the device.

3. Preliminary Results

Preliminary photodetector (PD) characterization, in terms of frequency response and receiver sensitivity, was done on stand-alone single photodetector test structures fabricated with the receivers, shown on the left side of Fig. 1 (b). The frequency response was measured with the LCA (Lightwave Component Analyzer) output coupled into the PD with a lensed fiber. The PD was contacted with a GSG RF probe and reversed biased through a bias tee. The RF signal from the PD was connected to the LCA through the bias tee. Fig. 2(a) shows the normalized response of the

photodetectors of lengths 10-30 μm , with 3dB bandwidth ranging from 23 to 28 GHz. Fig. 2(b) shows the effect of increasing reverse bias on a 30 μm long photodetector.

To measure PD sensitivity, an NRZ-OOK signal with a PBRs $2^{31}-1$ pattern was amplified by an EDFA, attenuated by a variable optical attenuator, and then coupled into the PD with a lensed fiber. The PD was reversed biased at -3V with a bias tee and the RF signal from the PD was sent through the bias tee to the BERT or scope. Fig. 3(a) shows the NRZ-OOK BER curves at 20, 35, 30, and 35 Gb/s, assuming a 10 dB coupling loss from fiber to chip, and receiver sensitivity of approximately -0.5 dBm at 20 Gb/s and 3.5 dBm at 25 Gb/s. Since the PD is neither preamplified nor postamplified, receiver sensitivity is low. Low sensitivity is also attributed to a small ($<1\mu\text{m}$) overlap of the p-metal layer and n-contact, causing a short that results in lower responsivity and a high dark current. The NRZ-OOK eye diagrams at 25, 30, and 40 Gb/s are shown in Fig 3(b) with 15 dBm of input power measured at the lensed fiber.

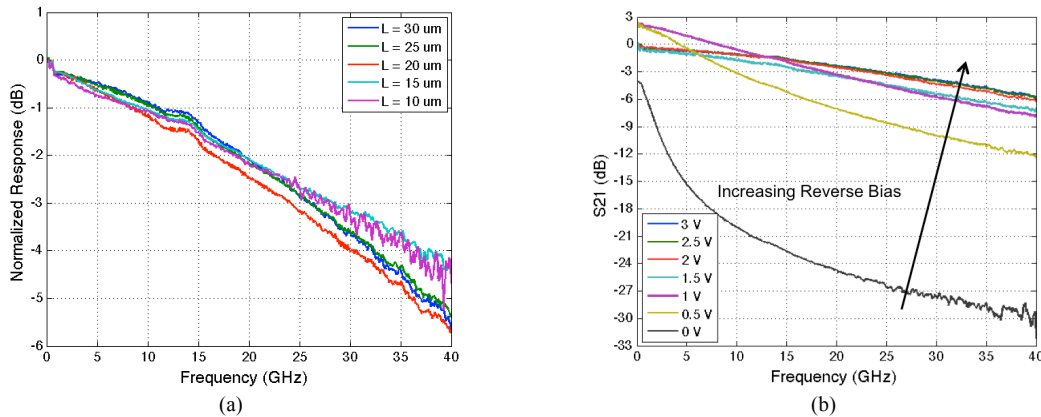


Figure 2. (a) Normalized photodetector response for detector lengths $L=10, 15, 20, 25, 30 \mu\text{m}$ at 3V reverse bias and (b) response varying reverse bias for detector length $L=30 \mu\text{m}$.

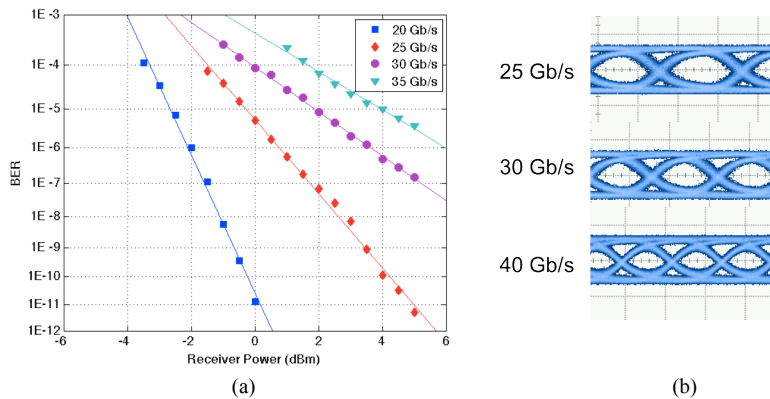


Figure 3. (a) NRZ-OOK BER curves with a PBRs $2^{31}-1$ pattern. The receiver power is the estimated power at the PD, assuming 10 dB coupling loss. (b) NRZ-OOK Eye diagrams at 25, 30, and 40 Gb/s (20 ps/div) with 15 dBm at lensed fiber (5 dBm to PD assuming 10 dB coupling loss)

3. Conclusions and Future Work

Preliminary photodetector measurements performed on stand-alone single photodetector test structures verify PD operation at 25 Gb/s. Future work includes characterization of the delay interferometer, balanced photodiodes, and the demonstration of this device as a receiver with 50 Gb/s DQPSK data.

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4. References

- [1] Winzer, P. J., Essiambre, R.-J., "Advanced Modulation Formats for High-Capacity Optical Transport Networks," *Journal of Lightwave Technology*, , vol.24, no.12, pp.4711-4728, Dec. 2006
- [2] Doerr, C.R.; Long Chen, "Monolithic PDM-DQPSK receiver in silicon," *Optical Communication (ECOC), 2010 36th European Conference and Exhibition on*, , vol., no., pp.1-3, 19-23 Sept. 2010
- [3] H. Park, A. W. Fang, D. Liang, Y.-H. Kuo, H.-H. Chang, B. R. Koch, H.-W. Chen, M. N. Sysak, R. Jones, and J. E. Bowers, *Advances in Optical Technologies*, Article ID 682978, 2008
- [4] H.-H. Chang, Y.-H. Kuo, R. Jones, A. Barkai, J. E. Bowers, Integrated Hybrid Silicon Triplexer, *Optics Express*, Vol. 18, Issue 23, pp. 23891-23993 (2010)